# What You Don't Know You Don't Know About (Hot) Water 

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## Goal of this Session:

- Identify at least 5 things you didn't know you didn't know about (hot) water
- Any specific topics you want me to address?
- Are you ready?


## 1. Water Heaters Have Air Filters

- Well, not all of them, but a very large and growing percentage
- Atmospheric Gas-fired Storage Heaters
- Flammable Vapor Ignition Resistance (FVIR)
- Closed combustion chamber, screen with tiny air holes, easily clogged with dust and lint
- Large particle screen surrounds the bottom of the heater
- Electric Heat Pump Water Heaters
- Filter on the inlet side of the air path through the heat pump coils.
- Filters need to be cleaned regularly!


## 2. Fixed vs. Variable Orifices

- Fixed Orifice:
- High pressure: High flow rate
- Low pressure: Low flow rate
- Before 2000, practically all fixture fittings and appliances
- Pressure Compensating Aerators
- Adjusts flow rate to compensate for available pressure
- Almost the same flow rate for all pressures above 20-25 psi
- Ramped up from 2000-2012 for showerheads
- Today more than $90 \%$ and many faucet aerators


## Pressure Compensating Aerators - 1



## Pressure Compensating Aerators - 2



## Pressure Compensating Aerators - 3



## Pressure Compensating Aerators - 4



A pressure
compensating flow regulator maintains a constant flow regardless of variations in line pressure thereby optimizing system performance and comfort of use at all pressures.

## 3. (Hot) Water Flow in Buildings

- What percent of the time does water flow through the meter into the building?
- Most normal condition is off - zero flow!
- Depending on occupancy, more than $96 \%$ of the time
$-2^{\text {nd }}$ most normal is 1 fixture fitting or appliance
- Probably cold, say a toilet
- Of the remaining $4 \%$, this happens more than $3.9 \%$ of the time
- Hot water is roughly half of this.
- Flows greater than 3 gpm occur less than $0.1 \%$ of the time


## 3. (Hot) Water Flow in Buildings (cont.)

- Pipe sizing rules were written down in the 1940s
- Pressure and temperature balanced shower valves became widely available in the 1980s
- Pressure compensating orifices became widely available in the 2010s
- These two devices mitigate many of this issues that occurred with peak flow rates
- Relatively constant, safe flow rates for showers and faucets
- Little impact on the fill rates for toilets, tubs and machines.
- Let's use these technologies to help with revising the rules for pipe sizing.


## Water Consumption 1980-2017

| Water-using Fixture or Appliance | 1980s Water Use (typical) | 1990 <br> Requirement (maximum) | EPAct 1992 Requirement (maximum) | 2009 Baseline Plumbing Code (maximum) | "Green Code" Maximums (2017 CALGreen) | \% Reduction in avg water use since 1980s |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Residential Bathroom Lavatory Faucet | $3.5+\mathrm{gpm}$ | 2.5 gpm | 2.2 gpm | 2.2 gpm | 1.2 gpm | 66\% |
| Showerhead | $3.5+\mathrm{gpm}$ | 3.5 gpm | 2.5 gpm | 2.5 gpm | 1.8 gpm | 49\% |
| Residential ("private") <br> Toilet | 5.0+ gpf | 3.5 gpf | 1.6 gpf | 1.6 gpf | 1.28 gpf | 74\% |
| Commercial ("public") <br> Toilet | 5.0+gpf | 3.5 gpf | 1.6 gpf | 1.6 gpf | 1.28 gpf | 74\% |
| Urinal | $\begin{aligned} & 1.5 \text { to } 3.0+ \\ & \mathrm{gpf} \end{aligned}$ | $\begin{aligned} & 1.5 \text { to } 3.0+ \\ & \mathrm{gpf} \end{aligned}$ | 1.0 gpf | 1.0 gpf | 0.125 gpf | 96\% |
| Commercial Lavatory Faucet | $3.5+\mathrm{gpm}$ | 2.5 gpm | 2.2 gpm | 0.5 gpm | 0.5 gpm | 86\% |
| Food Service Pre-Rinse Spray Valve | $5.0+\mathrm{gpm}$ | No requirement | $\begin{gathered} 1.6 \mathrm{gpm} \\ (\text { EPAct 2005) } \end{gathered}$ | No requirement | 1.3 gpm | 74\% |
| Residential Clothes Washing Machine | 51 gallons per load | No requirement | 26 gallons per load (2012 std) | No requirement | 12.6 gallons per load (Energy Star) | 75\% |
| Residential Dishwasher | 14 gallons per cycle | No requirement | 6.5 gallons per cycle (2012 std) | No requirement | 3.5 gallons per cycle (Energy Star) | 75\% |

From 1980 to 2017: Reductions range from 49 to 96\%

## Right-size the Supply Piping

## 2018 IAPMO Uniform Plumbing Code (UPC)

- Appendix M, Peak Water Demand Calculator
- Single- and multi-family homes with water-conserving plumbing fixtures, fixture fittings and appliances
- In general, can expect reduction of one nominal diameter.
- Going smaller than 0.5 inch nominal?
- Pay attention to velocity and residual pressure
- http://www.iapmo.org/water-demand-calculator/


## 4. Time-to-Tap and Volume-until-Hot

- More water than is in a pipe comes out of it before hot water arrives. How much more?
- Carl Hiller measured this in the early 2000s for $3 / 8$ to $3 / 4$ inch copper, CPVC and PEX piping
- Zhang recently reviewed the data and has found that for flow rates of 0.5 to 2 gpm in $3 / 4$ inch pipe, 1.5-2.5 times the pipe volume comes out before hot water (>105F) comes out the other end. Roughly 2:1.
- Conclusion: if you want hot water to arrive within 10 seconds, make sure there is no more than 5 seconds of volume in the pipe between the source of hot water and the use.


## How Long Should We Wait?

| Volume in <br> the Pipe <br> (ounces) | Minimum Time-to-Tap (seconds) at Selected Flow Rates |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mathbf{0 . 2 5} \mathbf{~ g p m}$ | $\mathbf{0 . 5} \mathbf{~ g p m}$ | $\mathbf{1} \mathbf{g p m}$ | $\mathbf{1 . 5} \mathbf{~ g p m}$ | $\mathbf{2 g p m}$ | $\mathbf{2 . 5} \mathbf{~ g p m}$ |
| $\mathbf{2}$ | 4 | 1.9 | 0.9 | 0.6 | 0.5 | 0.4 |
| $\mathbf{4}$ | 8 | 4 | 1.9 | 1.3 | 0.9 | 0.8 |
| $\mathbf{8}$ | 15 | 8 | 4 | 2.5 | 1.9 | 1.5 |
| $\mathbf{1 6}$ | 30 | 15 | 8 | 5 | 4 | 3 |
| $\mathbf{2 4}$ | 45 | 23 | 11 | 8 | 6 | 5 |
| $\mathbf{3 2}$ | 60 | 30 | 15 | 10 | 8 | 6 |
| $\mathbf{6 4}$ | 120 | 60 | 30 | 20 | 15 | 12 |
| $\mathbf{1 2 8}$ | 240 | 120 | 60 | 40 | 30 | 24 |

## Cut the volume in half to get these times!

ASPE Time-to-Tap Performance Criteria

|  | Acceptable Performance | $1-10$ seconds |
| :--- | :--- | ---: |
|  | Marginal Performance | $11-30$ seconds |
|  | Unacceptable Performance | $31+$ seconds |

## 5. Pressure Drop Through Pipe and Fittings

- Many materials and types of fittings
- Calculations vs. measured data
- Are the data we use representative of present day materials and fittings?

From the current ASHRAE Fundamentals Pipe Sizing chapter

- Hegberg (1995) and Rahmeyer (1999a, 1999b) discuss the origins of some of the data shown in Tables 4 and Table 5.
- The Hydraulic Institute (1990) data appear to have come from Freeman (1941), work that was actually performed in 1895.
- The work of Giesecke (1926) and Giesecke and Badgett (1931, 1932a, 1932b may not be representative of current materials.


## Pressure Drop - 1

- Elbows widely spaced and close together
- Velocities from 1-12 feet per second
- So far, we have not yet measured any published numbers
- Are our measurements higher or lower than what is published? Yes!
- Do our numbers have the same trends as what is published? No!
- It matters if we want to right-size piping systems.


# Southern California Gas Company Hot Water Demonstration Lab Downey, CA 







## Pipe from $1 / 4$ inch to $3 / 4$ inch Nominal



Pipe from $1 / 4$ inch to $3 / 4$ inch Nominal


## 90 Degree Elbows



## Close-coupled Elbows



## Even Closer



## Pressure Drop Due to Elbows

|  | Equivalent Feet of 1/2" Tubing |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Water Velocity in Tubing Feet per Second |  |  |  |
| $9 \mathbf{0}^{\circ}$ Elbow Type | 2 FPS | 4 FPS | 5 FPS | 8 FPS |
| PEX Crimp Insert | 8.6 | 10.1 | 9.8 | 11.9 |
| PEX Poly SS Press | 7.9 | 8.9 | 8.9 | 9.6 |
| PEX Cold Expansion | 6.6 | 7.3 | 8.0 | 9.1 |
| CPVC (Std Elb) | 1.7 | 0.8 | 0.9 | 1.3 |
| Copper (Std Tight Elb) | 0.0 | 0.4 | 0.3 | 0.6 |

## Pressure Drop Due to Elbows

| Tight Spacing of <br> Elbows | Equivalent Feet of 1/2" Tubing |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Water Velocity in Tubing Feet per Second |  |  |  |
| $\mathbf{9 0} \mathbf{0}^{\circ}$ Elbow Type | 2 FPS | 4 FPS | 5 FPS | 8 FPS |
| PEX Poly SS Press | 7.9 | 8.9 | 9.6 |  |
| Tight Spacing | 8.4 | 10.8 | 11.7 |  |
|  |  |  |  |  |
| PEX Cold Expansion | 6.6 | 8.0 | 9.1 |  |
| Tight Spacing | 7.9 | 9.3 | 9.4 |  |
|  |  |  |  |  |
| CPVC (Std Elb) | 1.7 | 0.9 | 1.3 |  |
| Tight Spacing | 0.7 | 1.3 | 1.5 |  |
|  |  |  |  |  |

## Arcata Test Site














## Brass <br> Crimp <br> Elbow

Plastic
Crimp
Elbow

Plastic
Evopex
Elbow

## Pressure Drop (PSI) ( 16.25 feet 0.5 inch PEX)



2 fps 4 fps 6 fps 8 fps 10 fps Max Flow

## Pressure Drop (PSI) (0.5 inch Brass Elbow)



## Pressure Drop (PSI) (0.5 inch Plastic Elbow)


$2 \mathrm{fps} 4 \mathrm{fps} \quad 6 \mathrm{fps} \quad 8 \mathrm{fps} \quad 10 \mathrm{fps}$

## Pressure Drop (PSI) (0.5 inch Evopex)



## Pressure Drop (PSI) (0.5 inch Sharkbite w/inserts)



## Pressure Drop (PSI) ( 0.5 inch Sharkbite w/o inserts)



## Pressure Drop Summary



Didn't have enough available pressure to run 10 fps test

## Pressure Drop per Elbow (PSI)



## Equivalent Feet per Elbow (feet)



## Pressure Drop-2

- Is there a minimum radius of curvature through which there is no additional pressure drop other than that due to the length of the bend?
- Wouldn't that be the most water, pressure, energy and time efficient bend?
- Ask me about the Swoop ${ }^{\circledR}$


## 6. Viscosity of Hot and Cold Water

- What is the viscosity of hot water compared to cold water?
- Is the difference small or large?
- Cold water is 1.7-2.8 times more viscous than hot water for a wide range of temperatures typically found in buildings!
- It is almost as though there are 2 different fluids moving through the same pipe.
- Slippery hot water and sluggish cold water.
- This helps explain much of the extra volume and time to get hot water from the source to the use.


## Ratio of the viscosity of water at a range of typical temperatures

| Cold:Hot | $50: 120$ | $50: 140$ | $70: 120$ | $70: 140$ |
| :---: | :---: | :---: | :---: | :---: |
| Ratio | 2.31 | 2.76 | 1.73 | 2.06 |


| Legend | Regime | Re Range | 1-D Dispersive Transport |
| :--- | ---: | ---: | :--- |
|  | turbulent | $20,000<\operatorname{Re}$ | low (probably not important) |
|  | transition | $4,000<\operatorname{Re}<20,000$ | low to moderate (might be important) |
|  | critical | $2,000<\operatorname{Re}<4,000$ | moderate to high (likely to be important) |
|  | Iaminar | $0<\mathbf{R e}<2,000$ | high (important) |

## Calculating the Reynolds Number

| Re =0.03404Q/vD | Temp (F) | Viscosity (ft^2/s) |
| :--- | ---: | ---: |
| Flow, Q (gpm) | 50 | 0.000014063 |
| Viscosity, v (ft^2/s) | 60 | 0.000012075 |
| Diameter, D (in) | 70 | 0.000010503 |
|  | 80 | 0.00000925 |
|  | 90 | 0.000008234 |
|  | 100 | 0.000007392 |
|  | 110 | 0.000006682 |
|  | 120 | 0.000006075 |
|  | 130 | 0.000005551 |
|  | 140 | 0.000005102 |

## Reynolds Number: 70F

| Temp = 70 F / 21 C | Flow (gpm) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Diameter (in) | 0.25 | 0.50 | 1.0 | 1.5 | 2.0 | 2.5 | 3.0 | 3.5 | 4.0 | 5.0 |
| 0.250 | 3241 | 6482 | 12964 | 19446 | 25928 | 32410 | 38892 | 45374 | 51856 | 64820 |
| 0.375 | 2161 | 4321 | 8643 | 12964 | 17285 | 21607 | 25928 | 30249 | 34570 | 43213 |
| 0.500 | 1620 | 3241 | 6482 | 9723 | 12964 | 16205 | 19446 | 22687 | 25928 | 32410 |
| 0.625 | 1296 | 2593 | 5186 | 7778 | 10371 | 12964 | 15557 | 18149 | 20742 | 25928 |
| 0.750 | 1080 | 2161 | 4321 | 6482 | 8643 | 10803 | 12964 | 15125 | 17285 | 21607 |
| 1.00 | 810 | 1620 | 3241 | 4861 | 6482 | 8102 | 9723 | 11343 | 12964 | 16205 |
| 1.25 | 648 | 1296 | 2593 | 3889 | 5186 | 6482 | 7778 | 9075 | 10371 | 12964 |
| 1.5 | 540 | 1080 | 2161 | 3241 | 4321 | 5402 | 6482 | 7562 | 8643 | 10803 |
| 2.0 | 405 | 810 | 1620 | 2431 | 3241 | 4051 | 4861 | 5672 | 6482 | 8102 |
| 2.5 | 324 | 648 | 1296 | 1945 | 2593 | 3241 | 3889 | 4537 | 5186 | 6482 |
| 3.0 | 270 | 540 | 1080 | 1620 | 2161 | 2701 | 3241 | 3781 | 4321 | 5402 |
| 3.5 | 231 | 463 | 926 | 1389 | 1852 | 2315 | 2778 | 3241 | 3704 | 4630 |
| 4.0 | 203 | 405 | 810 | 1215 | 1620 | 2026 | 2431 | 2836 | 3241 | 4051 |
| 5.0 | 162 | 324 | 648 | 972 | 1296 | 1620 | 1945 | 2269 | 2593 | 3241 |
| 6.0 | 135 | 270 | 540 | 810 | 1080 | 1350 | 1620 | 1891 | 2161 | 2701 |
| 8.0 | 101 | 203 | 405 | 608 | 810 | 1013 | 1215 | 1418 | 1620 | 2026 |

## Reynolds Number: 140F

| Temp = 140 F / 60 C | Flow (gpm) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Diameter (in) | 0.25 | 0.50 | 1.0 | 1.5 | 2.0 | 2.5 | 3.0 | 3.5 | 4.0 | 5.0 |
| 0.250 | 6672 | 13344 | 26688 | 40031 | 53375 | 66719 | 80063 | 93407 | 106750 | 133438 |
| 0.375 | 4448 | 8896 | 17792 | 26688 | 35583 | 44479 | 53375 | 62271 | 71167 | 88959 |
| 0.500 | 3336 | 6672 | 13344 | 20016 | 26688 | 33359 | 40031 | 46703 | 53375 | 66719 |
| 0.625 | 2669 | 5338 | 10675 | 16013 | 21350 | 26688 | 32025 | 37363 | 42700 | 53375 |
| 0.750 | 2224 | 4448 | 8896 | 13344 | 17792 | 22240 | 26688 | 31136 | 35583 | 44479 |
| 1.00 | 1668 | 3336 | 6672 | 10008 | 13344 | 16680 | 20016 | 23352 | 26688 | 33359 |
| 1.25 | 1334 | 2669 | 5338 | 8006 | 10675 | 13344 | 16013 | 18681 | 21350 | 26688 |
| 1.5 | 1112 | 2224 | 4448 | 6672 | 8896 | 11120 | 13344 | 15568 | 17792 | 22240 |
| 2.0 | 834 | 1668 | 3336 | 5004 | 6672 | 8340 | 10008 | 11676 | 13344 | 16680 |
| 2.5 | 667 | 1334 | 2669 | 4003 | 5338 | 6672 | 8006 | 9341 | 10675 | 13344 |
| 3.0 | 556 | 1112 | 2224 | 3336 | 4448 | 5560 | 6672 | 7784 | 8896 | 11120 |
| 3.5 | 477 | 953 | 1906 | 2859 | 3813 | 4766 | 5719 | 6672 | 7625 | 9531 |
| 4.0 | 417 | 834 | 1668 | 2502 | 3336 | 4170 | 5004 | 5838 | 6672 | 8340 |
| 5.0 | 334 | 667 | 1334 | 2002 | 2669 | 3336 | 4003 | 4670 | 5338 | 6672 |
| 6.0 | 278 | 556 | 1112 | 1668 | 2224 | 2780 | 3336 | 3892 | 4448 | 5560 |
| 8.0 | 208 | 417 | 834 | 1251 | 1668 | 2085 | 2502 | 2919 | 3336 | 4170 |

## 7. Converting Volume to Height

Most of us are between 5'-7' tall. This means we are roughly equal to:

- $1 / 8^{\prime \prime}$ pipe: 1 shot of liquor (1 ounce)
- $1 / 4$ " pipe: A "double" of liquor (2 ounces)
- $3 / 8^{\prime \prime}$ pipe: 1 glass of wine (4-6 ounces)
- 1/2" pipe: 1 cup of water (8 ounces)
- 3/4" pipe: 1 pint of beer (16 ounces)
- 1" pipe: 1 bottle of wine ( 750 ml )


## Length of Pipe that Holds 8 oz of Water

|  | 3/8" CTS | 1/2" CTS | 3/4" CTS | 1" CTS |
| :---: | :---: | :---: | :---: | :---: |
|  | ft/cup | ft/cup | ft/cup | ft/cup |
| "K" <br> copper | 9.48 | 5.52 | 2.76 | 1.55 |
| "L" <br> copper | 7.92 | 5.16 | 2.49 | 1.46 |
| "M" <br> copper | 7.57 | 4.73 | 2.33 | 1.38 |
| CPVC | N/A | 6.41 | 3.00 | 1.81 |
| PEX | 12.09 | 6.62 | 3.34 | 2.02 |

## Questions?

Given human nature, it is our job to provide the infrastructure that supports efficient behaviors.

